Contents

0.1	Abstract		
0.2	Kurzfassung		
1.	Introduction		
	1.1 1.2 1.3 1.4	Motivation Finite Difference Frequency Domain (FDFD) Method Anisotropic PML Absorbing Boundary Condition Internal Ports	5 9 10 11
2.	PML Parameters and Convergence		
	2.1 2.2 2.3	Motivation and General Considerations Overlapping PML Walls PML Cell Size	13 18 23
		2.3.1 Single PML Wall: Micro-strip Structure2.3.2 Multiple PML Walls: Patch Antenna2.3.3 Slot Antenna	24 29 34
	2.4 2.5 2.6	PML in Layered Media Improved Numerical Solver Conclusion	35 40 44
3.	Waveguide Port Simulation with PML		45
	3.1 3.2 3.3	Physical and Artificial Modes PML Modes and their Coupling to other Modes Conclusion	45 51 55
4.	Internal Port		
	4.1 4.2 4.3 4.4 4.5	Relaxation Current Internal Port Conduction Current Internal port (Line Current) Parasitic Effects of Conduction Current Internal Ports Analytical Formulation for the Parasitic Inductance Simulation with Conduction Current Internal Port	58 63 66 69 74
		4.5.1 T-junction 4.5.2 HEMT Structure	74 75
	4.6	Conclusion	79

5.	4-Quadrant Slot Antenna		
	5.1 5.2 5.3 5.4 5.5	Introduction Antenna Design Simulation Results with FDFD Realization and Measurement Results Conclusion	81 82 85 91 95
6.	Sumr	nary	96
7.	Appendix		99
	7.1 7.2 7.3 7.4 7.5 7.6 7.7 7.8	FDFD Discretization PML Modes and their Coupling to other Modes Excitation by Relaxation Current (Internal Port) Source Excitation by Conduction Current (Internal Port) Source Deembedding Conduction Current Internal Port Parasitics Excitation with Waveguide Ports Improvements in the F3D Solver Acronyms and symbols	99 100 105 107 109 112 114 116
8.	Literature		119
9	Curriculum Vitae		

0.1 Abstract

For EM simulations of complex MMIC structures, the usage of PML (Perfectly Matched Layer) absorbing boundary conditions is inevitable. PML provides a reflectionless open boundary condition and thus helps to keep the mesh size within a reasonable limit. On the other hand, structures completely enclosed by PML walls do not allow excitation by waveguide ports but require so-called internal ports. Such ports, which are introduced between two or more mesh points inside the structure, facilitate also to include lumped elements or entire networks thus enabling one to study active circuit, for instance.

This work treats both the PML boundary condition and the internal ports, in the framework of the frequency-domain Finite-Difference method (FDFD). It is shown that the presence of PML walls enlarges the magnitude range of the system matrix coefficients, encountered when calculating the fields. This makes the system matrix ill-conditioned and increases the number of iterations when solving the system and may even render this PML totally unusable for most practical applications. It is found that by avoiding any overlapping PML walls and by making the PML cell sizes the largest ones in the whole mesh the high count of the number of iterations can be lowered drastically.

The mode spectrum at waveguide ports with lateral PML walls consists of artificial PML and physical modes. We find that the coupling between PML modes and physical modes must be analyzed thoroughly in order to filter the artificial PML modes out in a reliable way.

Regarding the internal port, a line-current formulation proves to be the only practical choice. The parasitic inductances associated with it are found to be of significant influence. A closed-form expression for these inductances is developed in order to determine their values so that it can be deembedded from the results.

The optimized PML and internal port formulations are verified for the example of a 24 GHz slot antenna with integrated front-end MMIC, suitable for short range communications and sensor networks.